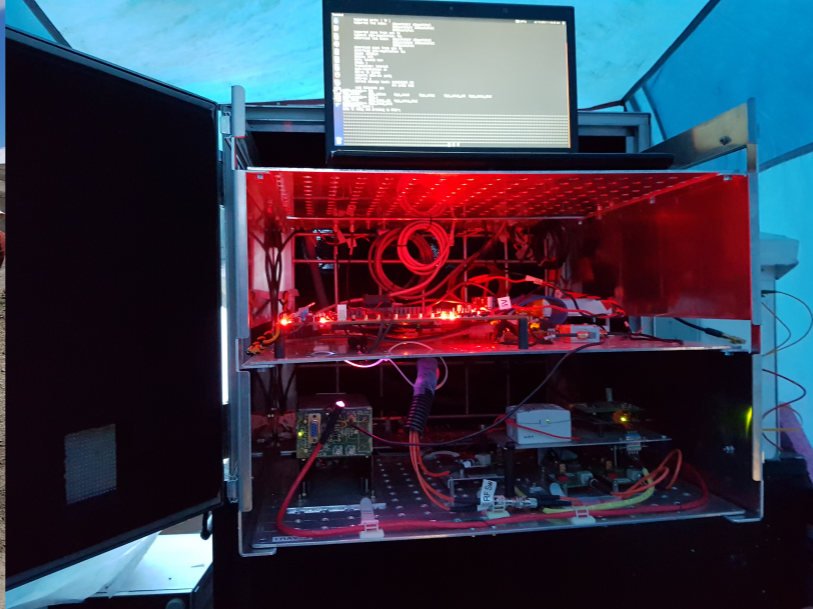


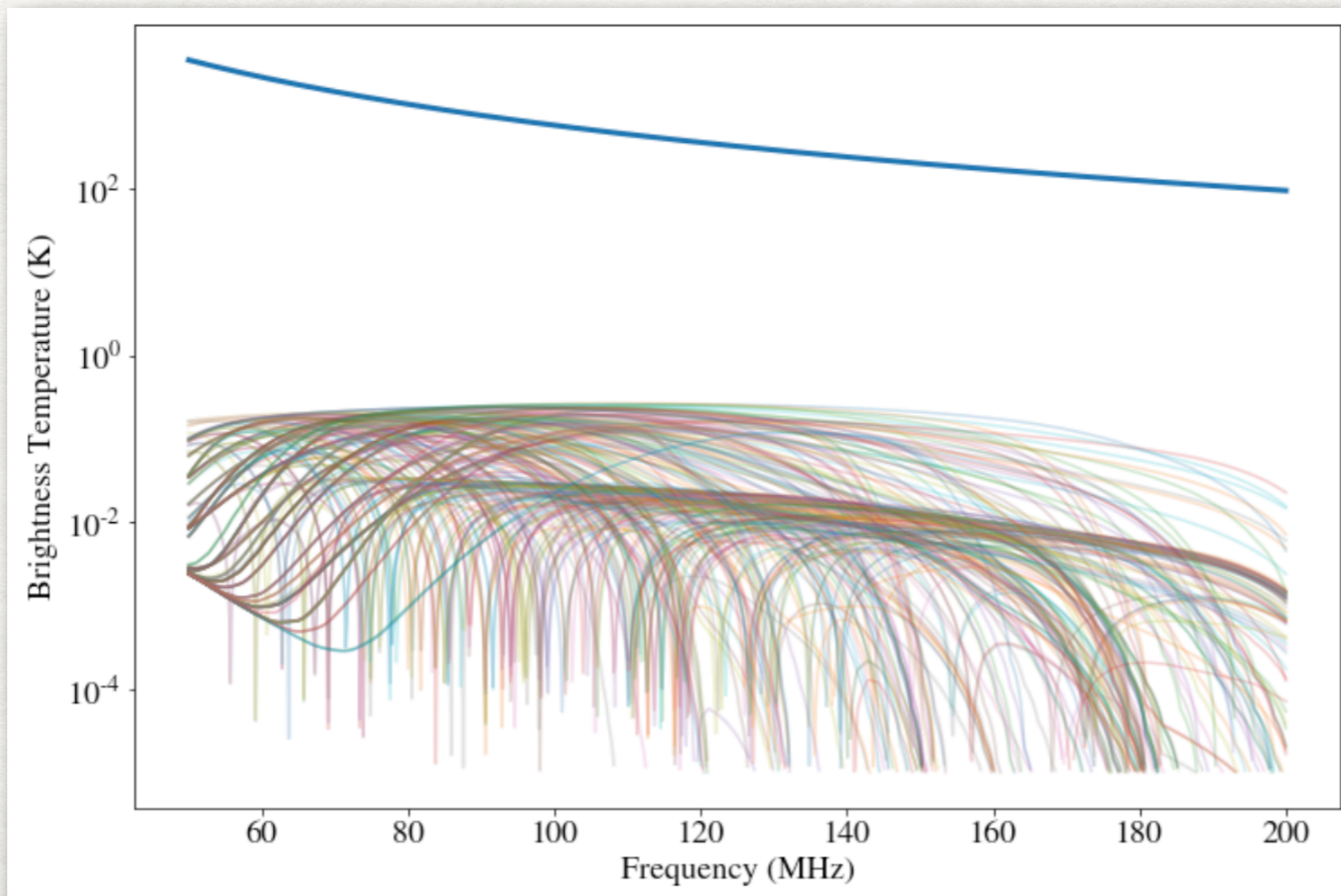
# SARAS: EVOLUTION OF SYSTEM DESIGN AND RELATED CHALLENGES

SAURABH SINGH  
ON BEHALF OF SARAS TEAM



# CHALLENGES

- Sensitivity is not a big concern!
- Thermal noise levels at 80 MHz, for 1 MHz channel bandwidth and 10 hours of integration  $\sim 10$  mK per frequency channel
- Systematics are far bigger challenges



Preserving the spectral smoothness of the foreground is the key!

Can spatial information be exploited?

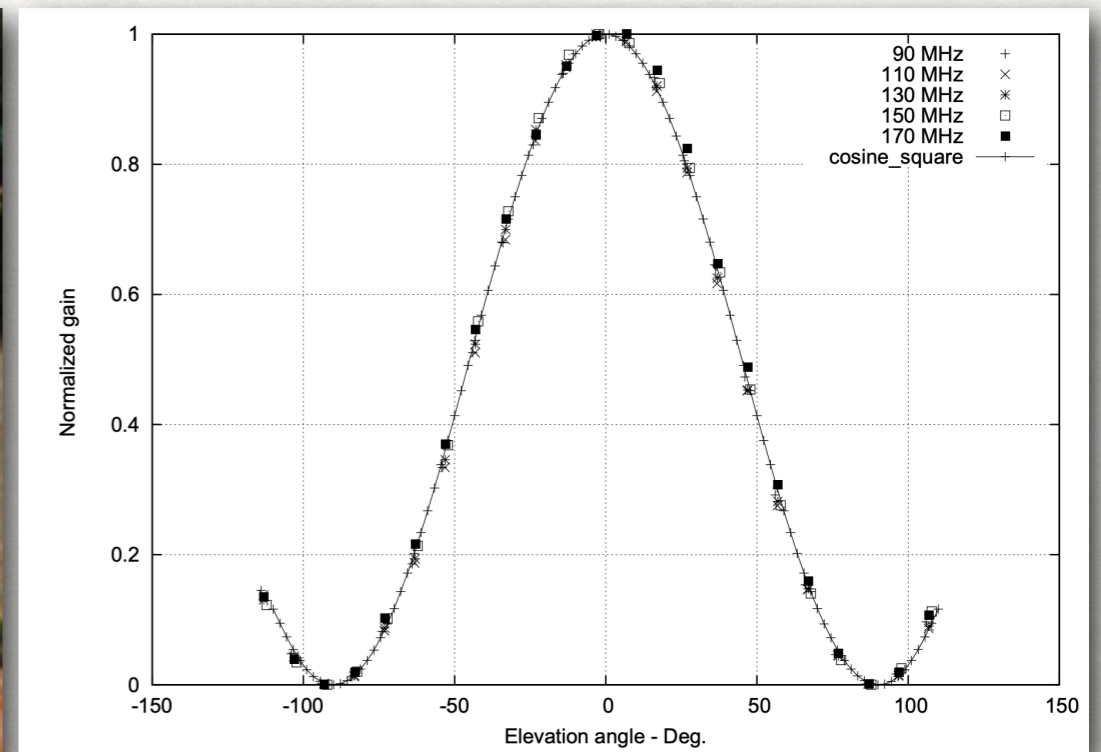
# CHALLENGES IN MODELING THE INSTRUMENT RESPONSE

- Antenna beam
  - Antenna transfer function
- } Often not calibratable  
Needs to be modeled externally
- Bandpass transfer function (analog + digital chain) → Mostly corrected with noise source injection
  - Additives from amplifiers + ground coupling → Often not calibratable  
Needs to be modeled externally

All these characteristics are frequency and (more or less) time/temperature dependent

# SARAS 1

- SARAS carried out first round of observations in 2012-2013
- It employed a fat-dipole antenna over absorber tiles

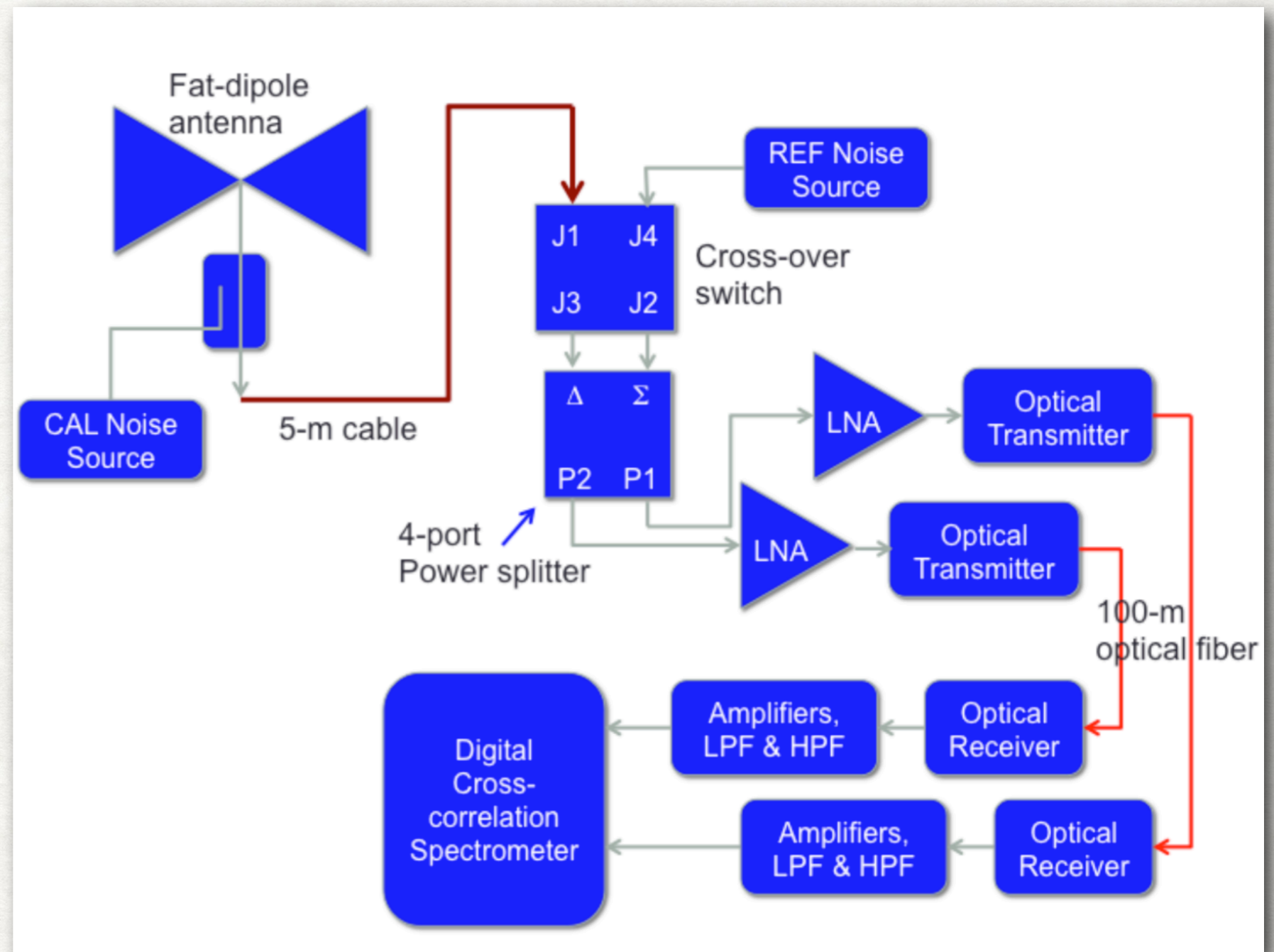


Return loss better than 15  
dB across the band

Image Courtesy:  
Patra et al. 2012, Raghunathan et al. 2012

# SARAS 1 RECEIVER

- SARAS 1 and 2 have similar analog receiver architecture and calibration schemes

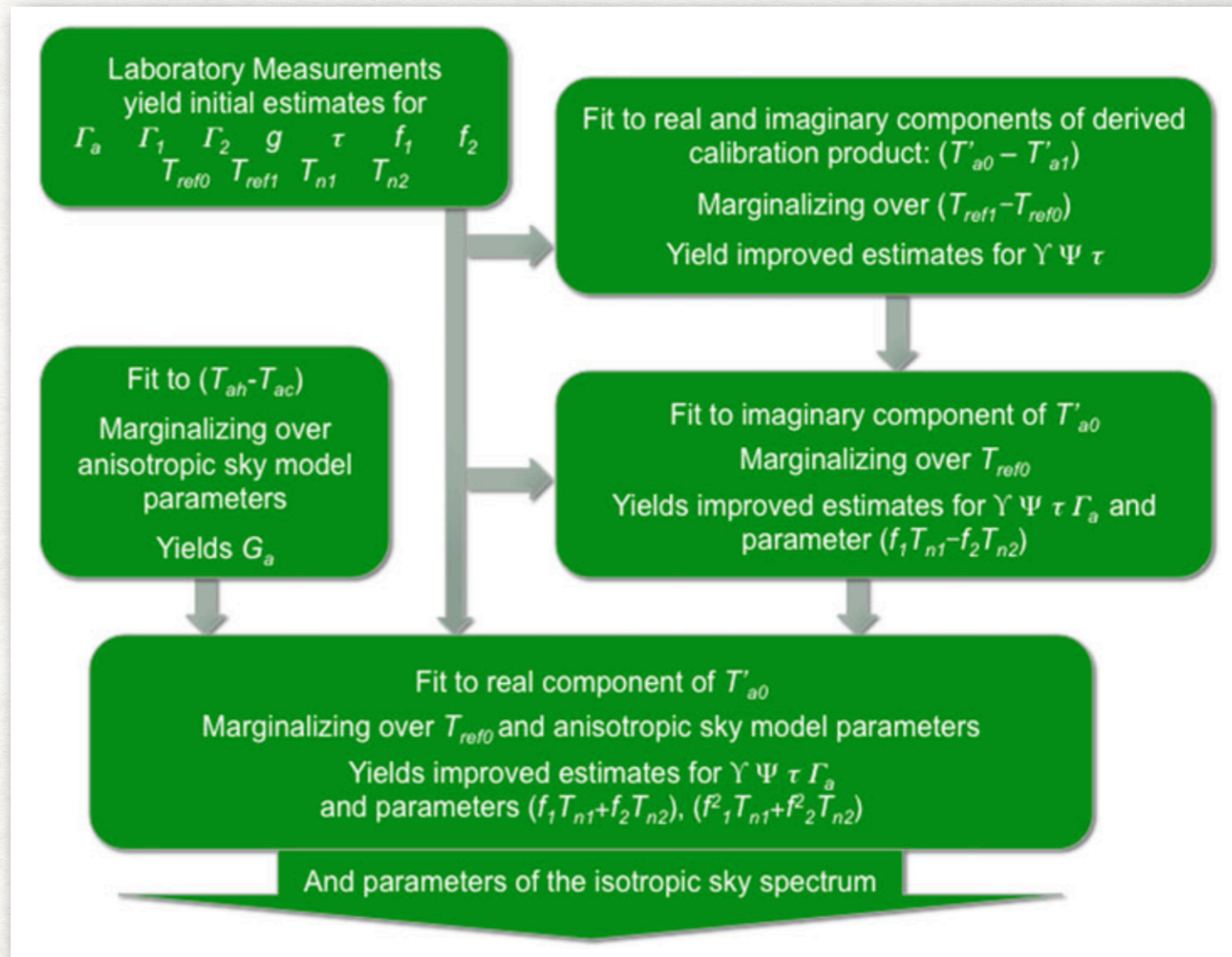


# SARAS (1&2) CALIBRATION

- **Bandpass calibration:** toggling between antenna and noise source every second
- **Absolute calibration:** tracking temperature of hot/cold loads via temperature loggers and radiometer measurements
- **Pseudo cross-correlation:** the signal path is split into two analog channels, phase-switched, and cross-correlated
  - Imaginary part of the cross-correlation contains systematics plus noise, which can be used to model them in the real component
  - Differencing of the data acquired in different system 'states' cancels out common-mode additives after splitting
  - Real part contains the sky signal that can be used for modeling EoR

# SARAS 1 MODELING

- Based on hierarchical modeling:
- The terms defining the instrument model are solved in the imaginary component of the measurement set and in calibration products
- Final stages of modeling involve sky terms





# SARAS 1 RESULTS

- Provided an improved absolute calibration for 150 MHz map all-sky map of Landecker & Wielebinski (1970)\*

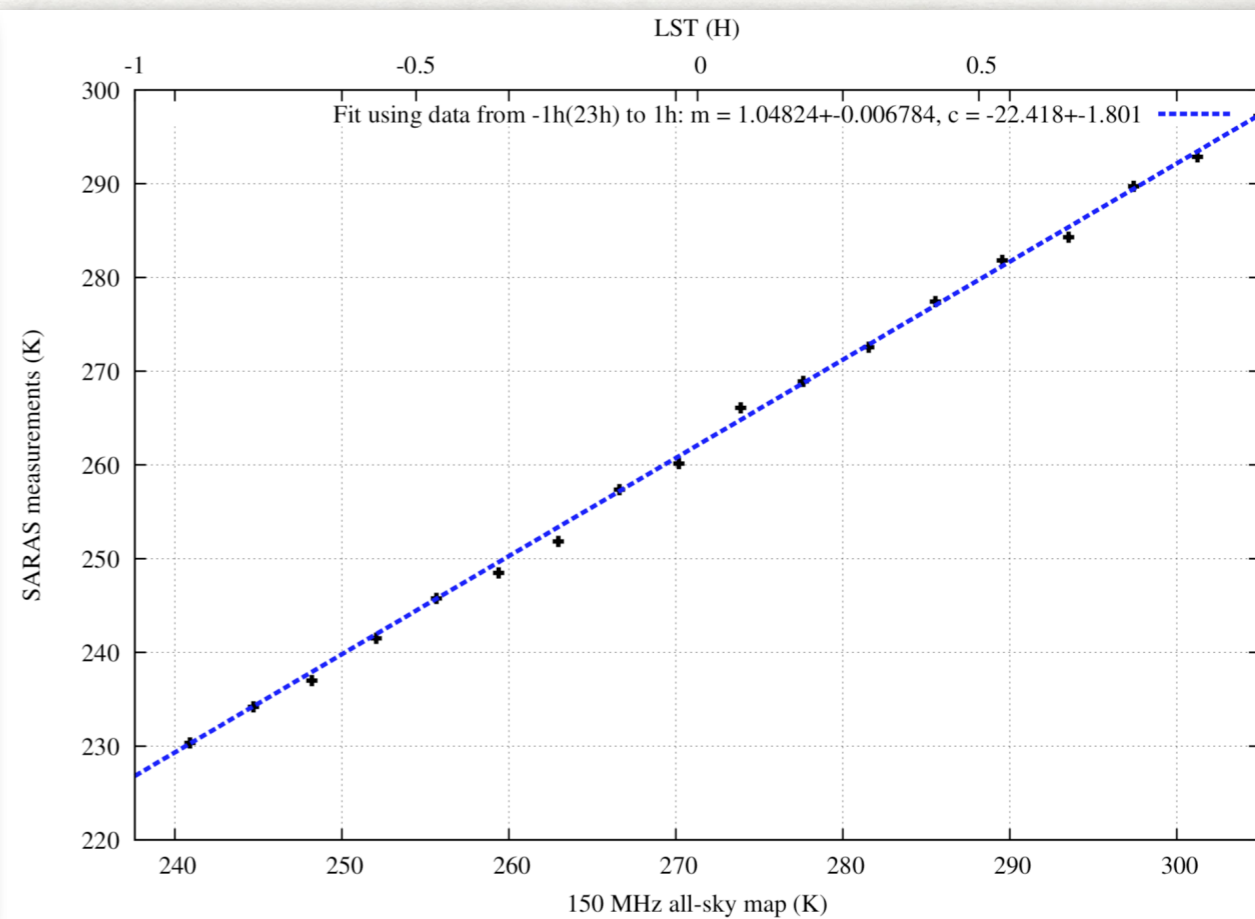
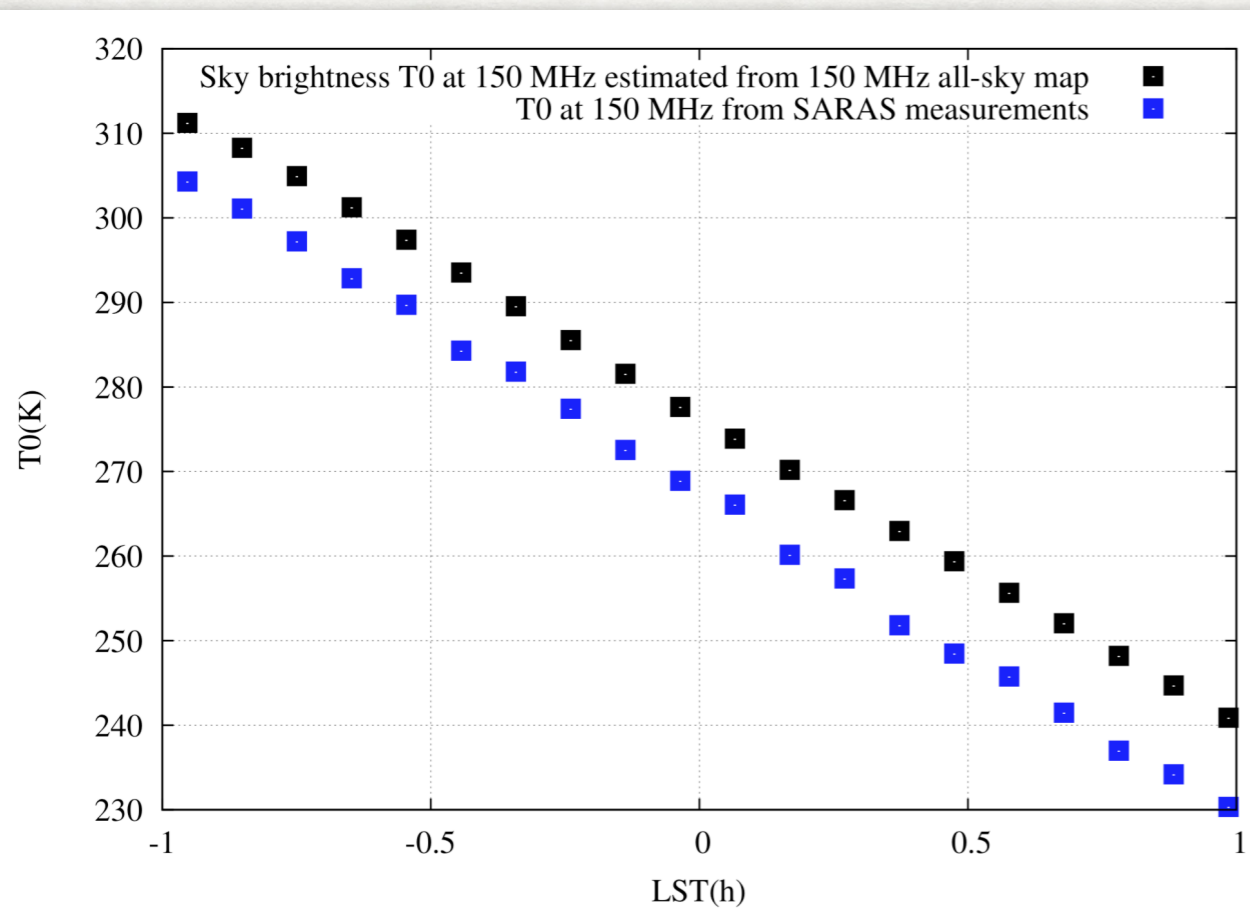


Image Courtesy:  
Patra et al. 2015

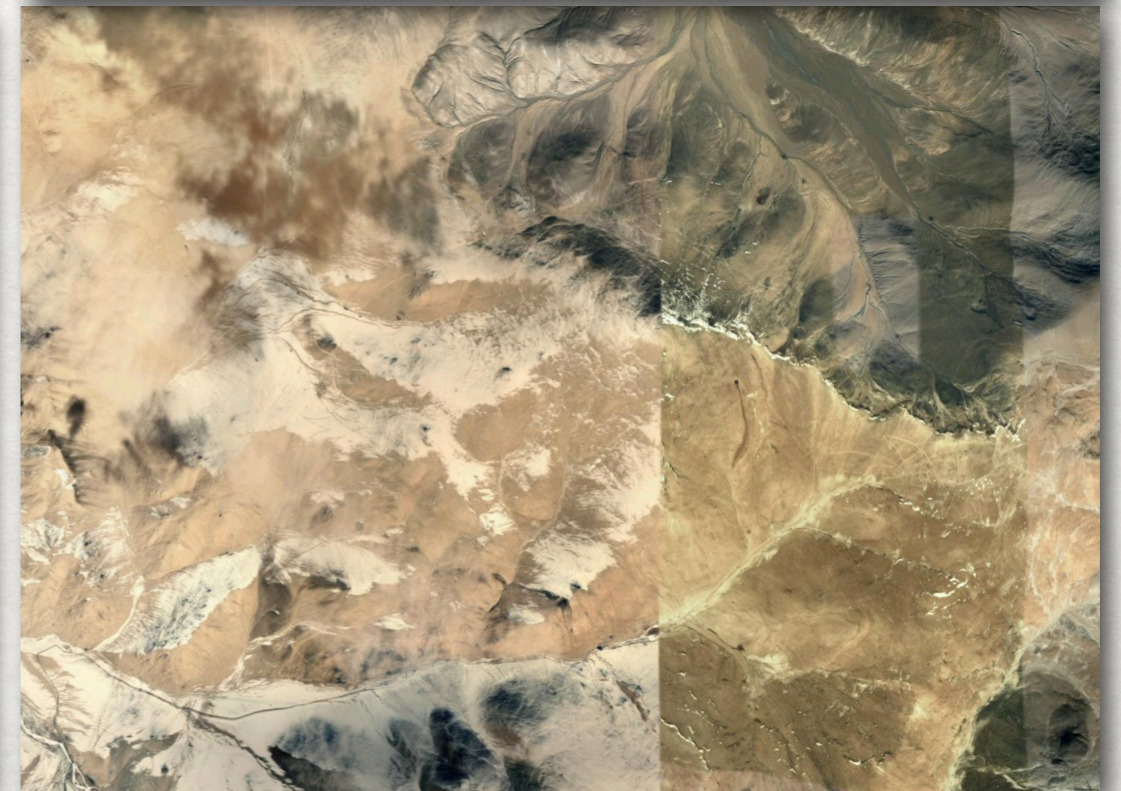
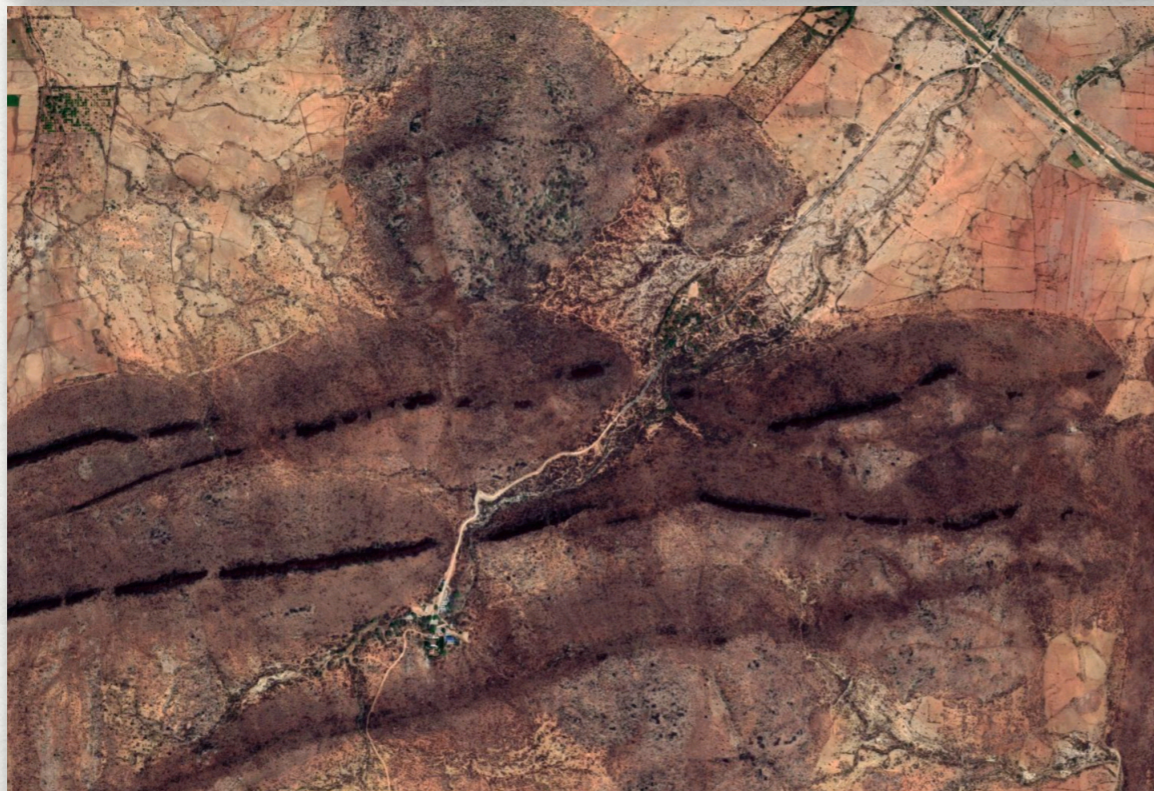
\*updated map available at:

[https://lambda.gsfc.nasa.gov/product/foreground/fg\\_all\\_sky150\\_mhzmap\\_get.cfm](https://lambda.gsfc.nasa.gov/product/foreground/fg_all_sky150_mhzmap_get.cfm)

# SARAS 1 CHALLENGES

- Radio Frequency Interference!
- Cable reflections (direct and multi-path), which were difficult to model to mK accuracy
- Absorbers, which had finite absorption, introduced another length scale corresponding to height between antenna and ground

# SITES OF OBSERVATIONS

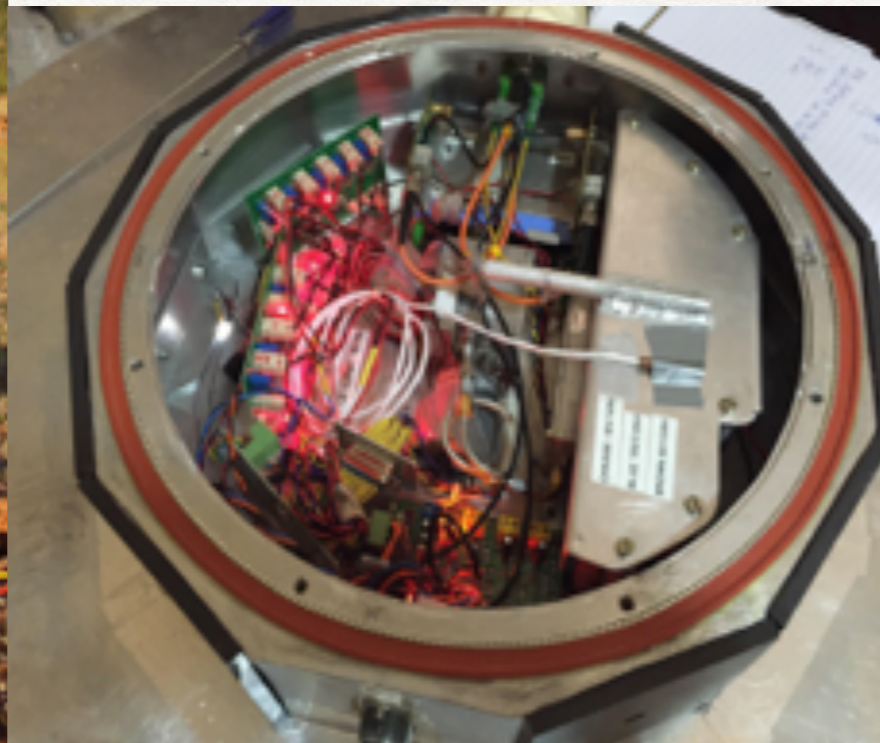
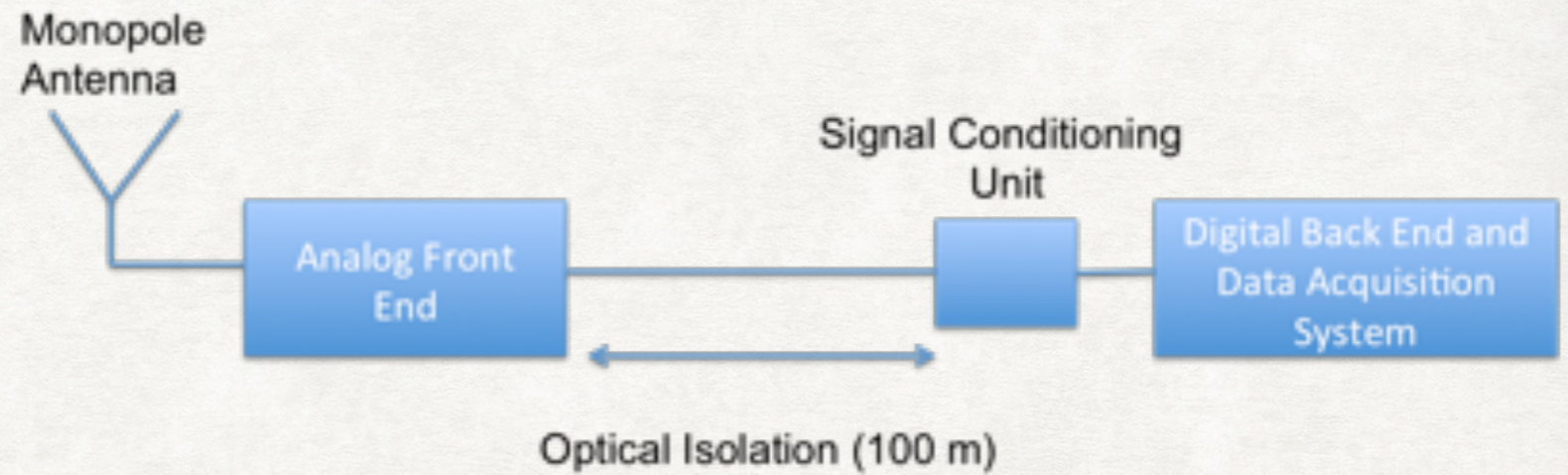


# SITES OF OBSERVATIONS

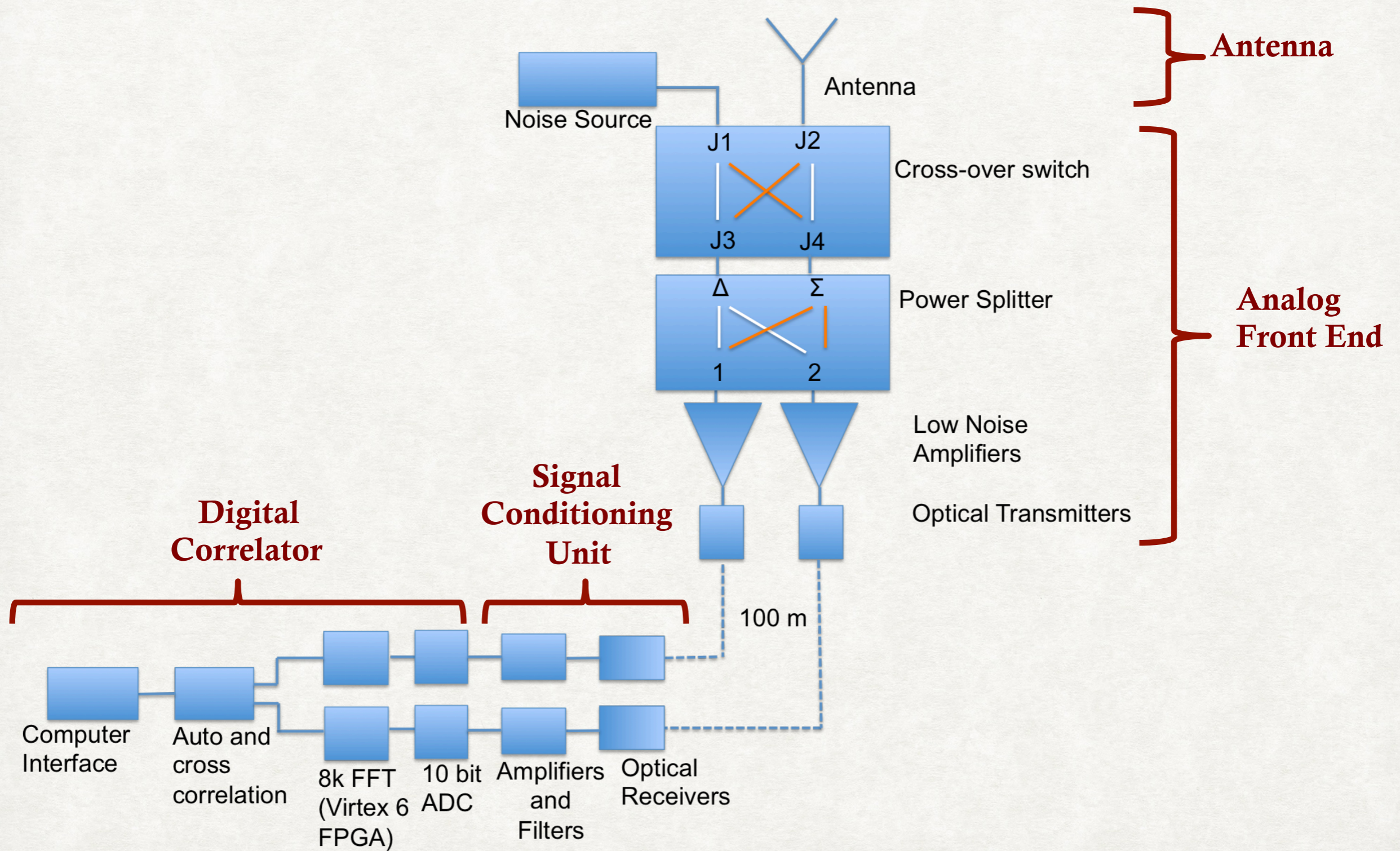


# SARAS 2

- SARAS 2 carried out observations over 2016-17 using a spherical monopole antenna



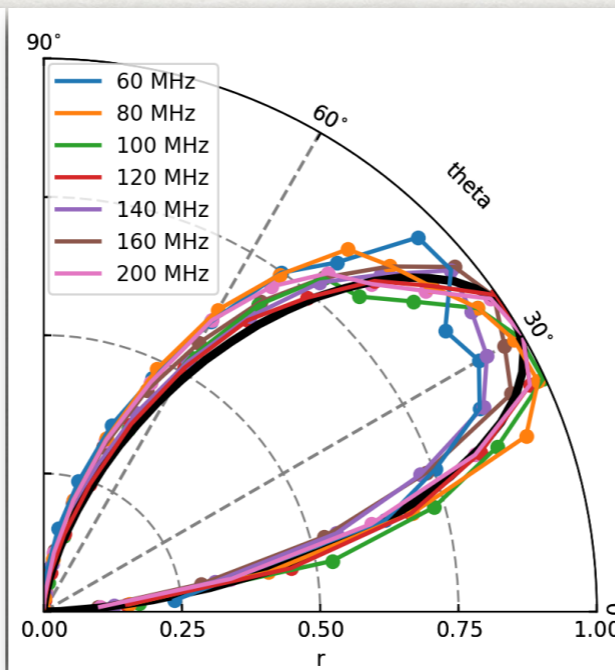
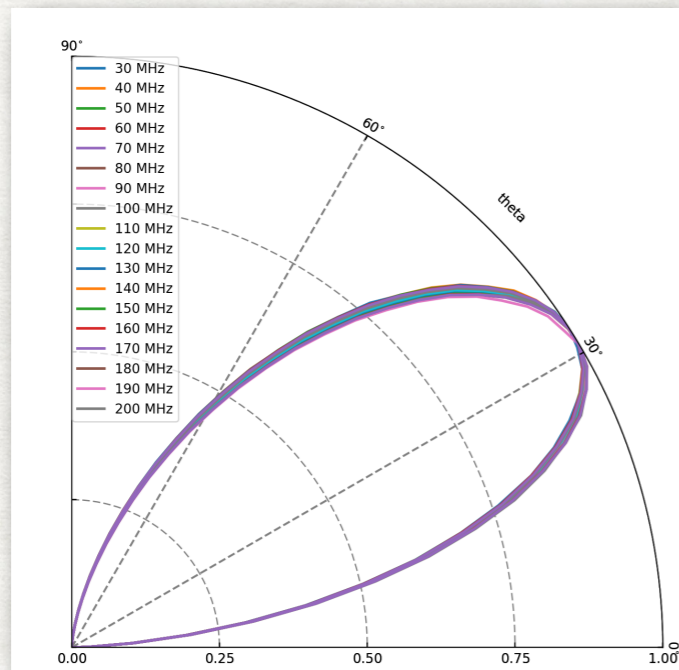
# SARAS 2 RECEIVER



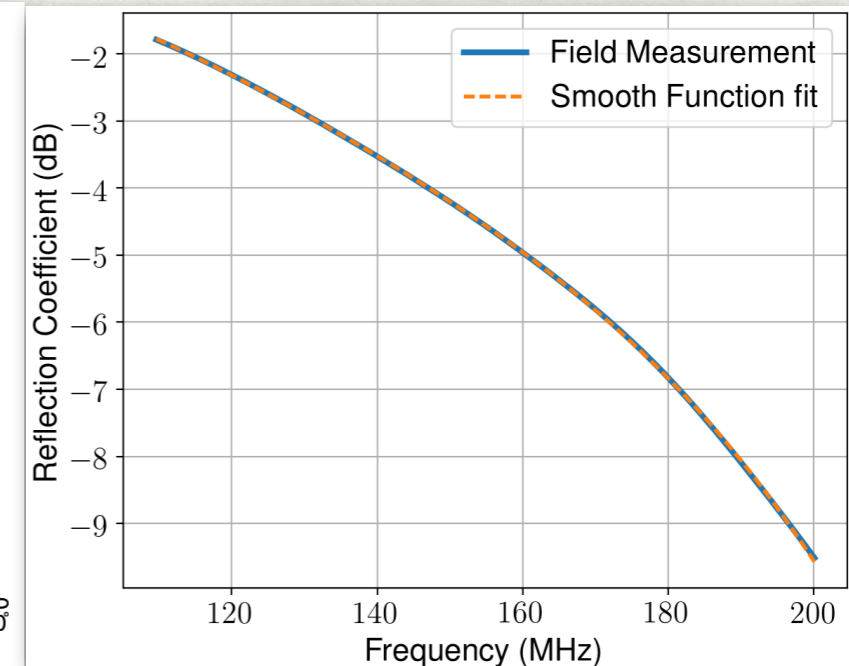
# CONTROL OF SYSTEMATICS

$$T'_A = \frac{\int_{\Omega} T_B(\theta, \phi) G(\theta, \phi) d\Omega}{\int_{\Omega} G(\theta, \phi) d\Omega}$$

Beam Pattern

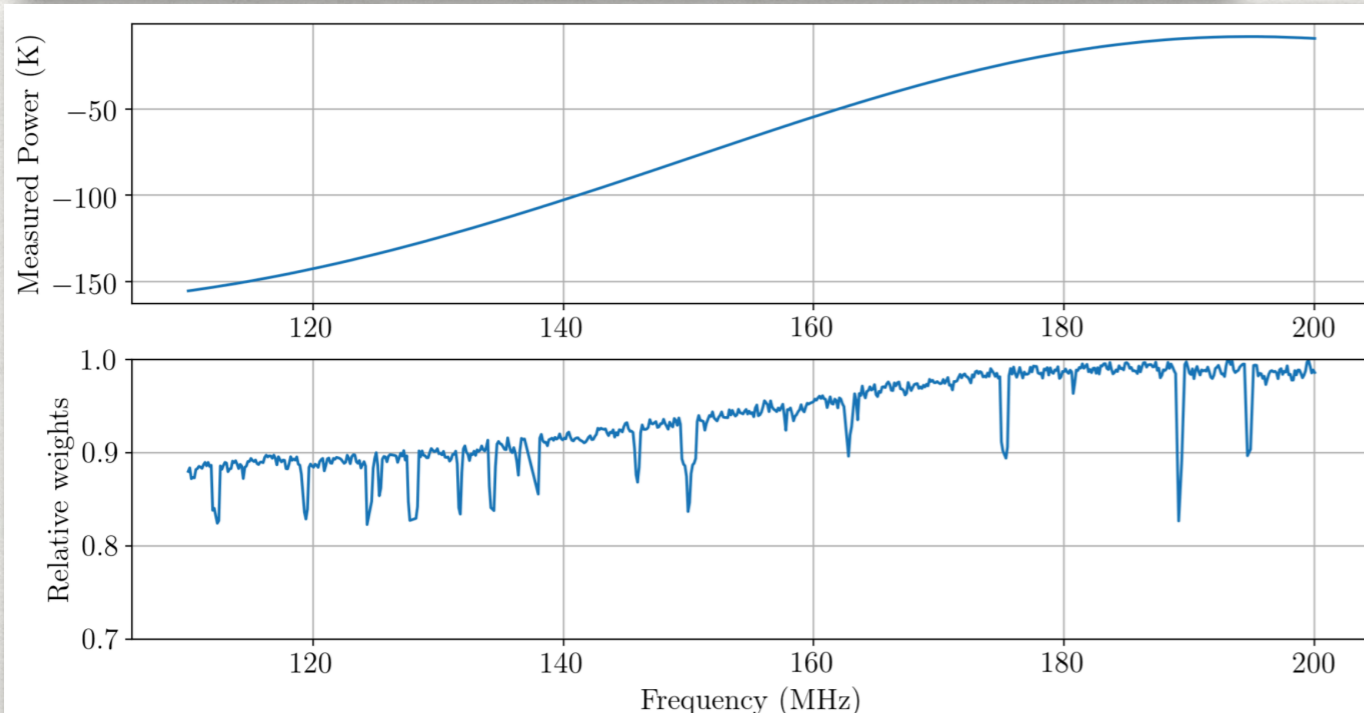
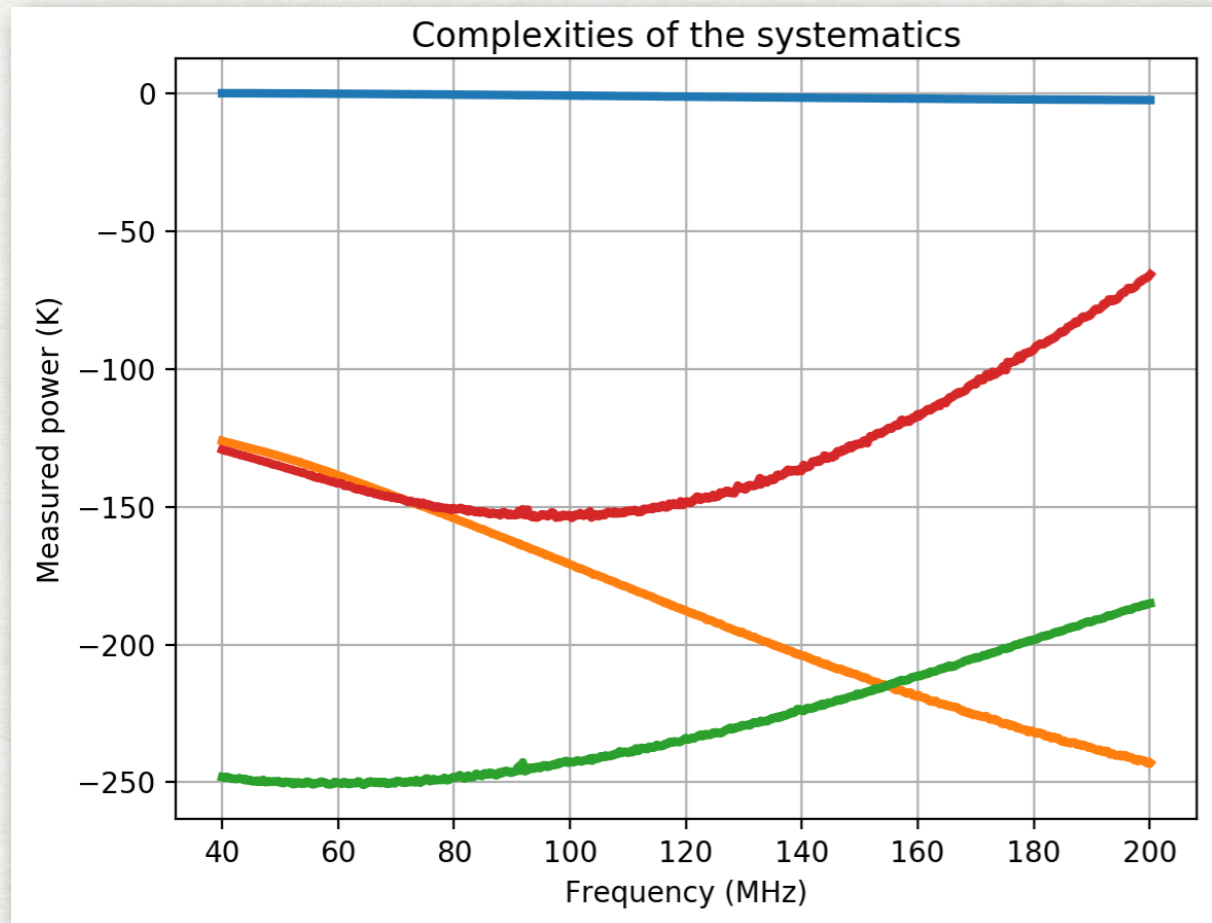


Reflection Coefficient



- Beam is achromatic
- Antenna transfer function is a smooth function of frequency, with no spectral wiggles
- Signals due to multipath propagation only result in a spectrally smooth component, owing to extreme miniaturization

# LAB AND FIELD RUNS



- Laboratory tests using loads with different spectral signatures
- Deployment in 2016-17 in Trans-Himalayan range, and Timbaktu Collective led to useful data ~60 hours
- Antenna Efficiency derived using observed data and sky model
- Efficiency enables analysis in 110-200 MHz



# SARAS 2 DATA MODELING

$$M(\nu) = F(\nu) + a \times S(\nu)$$

- Scale factor test
- Likelihood ratio test

Measurement Equation

Low order polynomials/  
smooth functions

$$T_{\text{meas}} = \left[ \left( \frac{C_1}{C_2} \right) T_A - T_{\text{REF}} + \left( \frac{C_{n1}}{C_2} \right) T_{N_1} + \left( \frac{C_{n2}}{C_2} \right) T_{N_2} \right], \text{ where}$$

$$C_1 = \left[ \sum_{l=0}^{\infty} |\gamma^{2l}| \sum_{m=0}^{\infty} \Re(\gamma^m e^{im\phi}) \right],$$

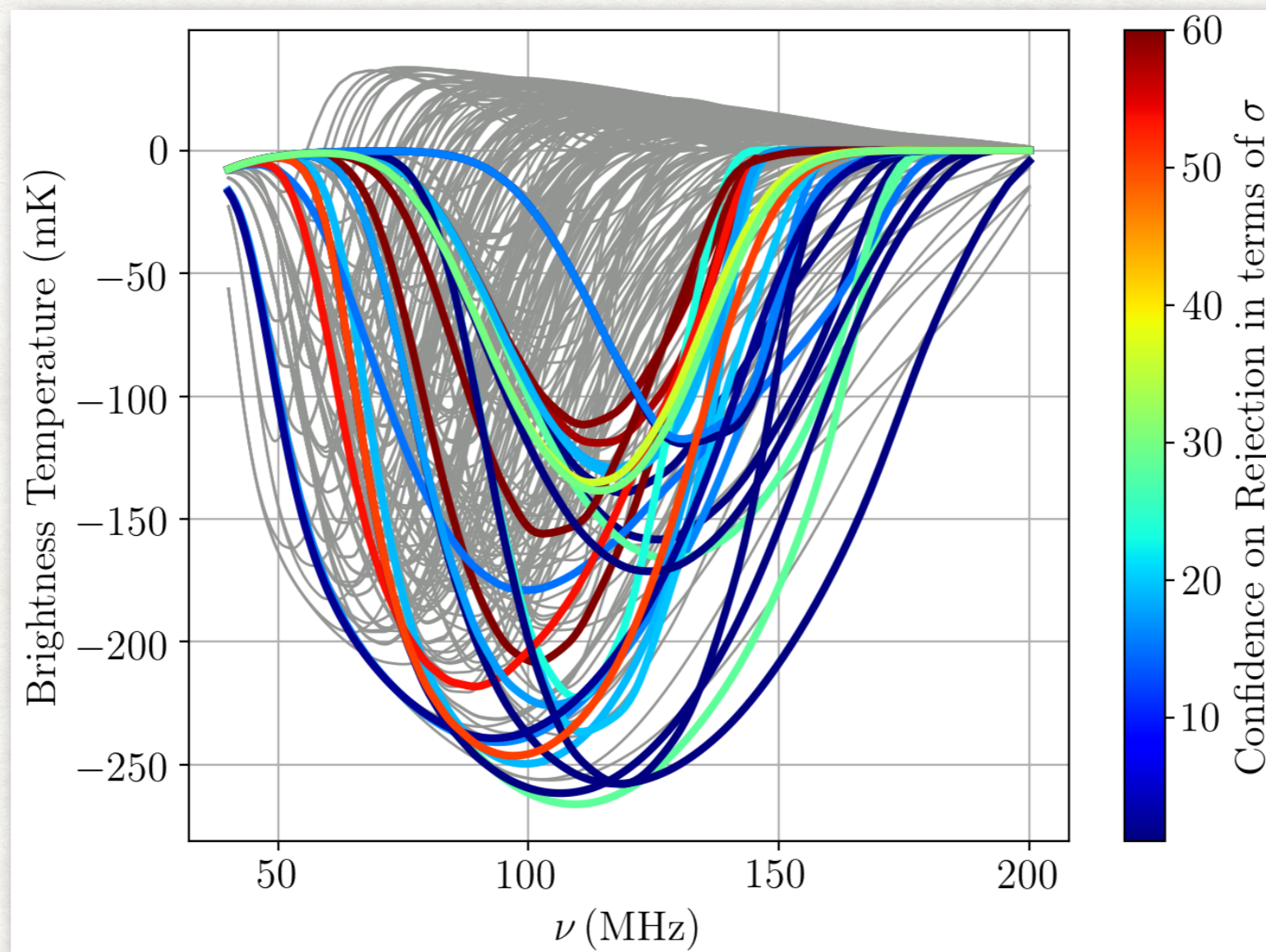
$$C_2 = \left[ 1 - |\psi|^2 \left( \sum_{l=0}^{\infty} \gamma^l e^{i(l+1)\phi} \right) \left( \sum_{m=0}^{\infty} \gamma^m e^{i(m+1)\phi} \right)^* + 2i\Im \left\{ \psi \left( \sum_{n=0}^{\infty} \gamma^n e^{i(n+1)\phi} \right) \right\} \right],$$

$$C_{n1} = f_1 \chi^* + f_1^2 |\chi|^2, \text{ and}$$

$$C_{n2} = f_2 \chi + f_2^2 |\chi|^2.$$

# SARAS 2 RESULTS

- SARAS 2 rejects the scenario of Rapid Reionization in tandem with either late X-ray heating or no heating



# SARAS 2 CHALLENGES

- The radiometer was system dominated over 50-100 MHz
- Low efficiency was not favorable to analyze data in 50-100 MHz
- It also implied larger coupling of ground radiation with the system

# TOWARDS LOW BAND UPGRADE...

- We upgraded the radiometer in 50-100 MHz band using scaled version of the antenna
- We conducted test observations with the upgraded system in Timbaktu Collective and near Indian Astronomical Observatory, Hanle (Leh-Ladakh, J&K) in 2018
- Currently, the analysis of ~100 hours of observations is limited by our ability to correct for ground radiation coupling to the antenna

# SUMMARY

- SARAS 1 provided an improved absolute calibration to 150 MHz sky map
- SARAS 2, with miniaturised design and no large length-scales, ruled out a class of theoretically predicted global 21-cm signatures
- Reduced sensitivity could not enable analysis in 50-100 MHz band
- Upgraded radiometer optimized for 50-100 MHz
- Next presentation would focus on our attempts at observing in this band